Effect of the Cable Capacitance of Long Control Cables on the Actuation of Contactors





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The problem of cable capacitance with long control cables also often occurs in large-scale installations such as with crane systems in container terminals.

## 0. Introduction:

The contactor is the most important switching device in industrial and commercial applications. Its importance has further increased due to the influence of automation. This has given rise to some significant advancements in the development of contactors, of which the user is often not aware. For example, the power required for switching has been considerably reduced in recent years due to the use of integrated actuation electronics.

Despite the many benefits made possible by the reduced power consumption, such as

- Energy savings
- Use of smaller control transformers
- Longer service life of control contacts

the reduced power requirements must be particularly taken into account with applications involving long control cables. Reliable contactor disconnection on actuation of the command device also depends on cable length, due to the cable capacitance between the command device and the contactor coil.

# 1. Cable capacitances

In certain circumstances, long control cables in AC actuated control circuits may prevent the disconnection of contactors due to the cable capacitance present.

Even if the command contacts are open, the coil current can still flow due to the cable capacitance so that the



No effect of cable capacitance  $C_L$  if the command contact is located close to the power supply. There may be a slight off-delay due to  $C_L$ .

contactor remains in the On position if sufficient sealing current is present.

The effect of cable capacitance depends on the design of the control current circuit:



Effect of cable capacitance  $C_L$  if the command contact is located away from the power supply. The coil current continues to flow even when the command contact is opened.

# **1.1 Capacitance of control cables**

A guide value for control cable capacitances between two conductors is approx.  $0.3\mu$ F per km for two-wire control, and approx.  $0.6\mu$ F per km between three conductors for three-wire control. The following equation should be used:

 $C_L = 0.3 (\mu F/km) \times I (km)$ Two-wire control (1.3)

 $C_L = 0.6 (\mu F/km) \times I (km)$ Three-wire control (1.4)

On disconnection,  $C_{L2}$  and  $C_{L3}$  are switched in parallel ( $C_{L1}$  is bridged by Q11).

However, the specific values depend on the cable used and may therefore vary. If necessary, obtain the cable capacitance from the manufacturer. When laying control cables together with other lines (e.g. in the cable duct), the cable capacitance can no longer be calculated. The capacitive currents must be measured.





Two-wire control:  $C_{L} = 0.3 (\mu F/km) \times I (km) (1.3)$ 



Three-wire control:  $C_L = 0.6 (\mu F/km) \times I (km) (1.4)$ 

# 2. Limit capacitance of a contactor

The maximum capacitance at which the contactor stays switched on in the new condition despite the off command can be calculated using the equation below:

$$C_{\max} = \frac{b}{1+a} \cdot \frac{P_{H} \cdot 10^{6}}{\omega \cdot U_{c}^{2}} \left[ \mu F \right] (2.0)$$

with

$$a = \frac{U_{AB}}{U_C} = 0.4$$
$$b = \frac{I_{AB}}{I_C} = 0.25...0.35$$

- $U_{AB}$  = minimum drop-off voltage in V
- I<sub>AB</sub> = Sealing current with a minimum drop-off voltage in A
- $P_{\rm H}$  = Rated sealing current of the contactor in VA
- $U_{\rm C}$  = Rated control supply voltage in V

At 50 Hz and a permissible rated control supply voltage 110% times rated voltage based on equation 2.0:

$$C_{\max} = 500 \cdot \frac{P_{H}}{U_{C}^{2}} \quad [\mu F]$$

At 60 Hz the values must be reduced by 20%.

# 3. Determining the maximum permissible control cable lengths

In order for a contactor to switch correctly,  $C_L$  must be less than  $C_{max}$ .

If equations (1.3) and (1.4) are related to equation (2.1), the following values are produced for 50 Hz networks:

$$I_{\text{perm}} = 1.7 \cdot 10^6 \cdot \frac{P_H}{U_c^2} \ [m]$$

Two-wire control (3.0)

$$I_{\text{perm}} = 0.85 \cdot 10^6 \cdot \frac{P_{H}}{U_c^2} \quad [m]$$

Three-wire control (3.1)

 $I_{perm}$  = maximum permissible control cable length in m.

With 60Hz networks the values for (3.0) and (3.1) must be reduced by 20%.



Permissible single control cable length with a rated actuation voltage of 110% UC in relation to the contactor sealing power

		Maximum permissible cable length in m for			
Competent	Sealing power VA	Two-wire control 50Hz	Three-wire control 50Hz	Two-wire control 60Hz	Three-wire control 60Hz
Uc = 230 V DILE(E); S(E)00 DILM7DILM15; DILA DILM17DILM32 DILM40DIL65 DILM80; DILM95 DILM115; DIL150 DILM185DILM250 DILM300DILM500 DILM580DILM1000 DILM1400 DILH12000	4.6 4 8 16 26 3.5 4.3 4.3 7.5 7.5 7.5	148 129 257 514 836 112 138 138 241 241 482	74 64 129 257 418 56 69 69 121 121 241	118 103 206 411 668 90 111 111 193 193 386	59 51 103 206 334 45 55 55 96 96 96 193
Uc = 120 V DILE(E); S(E)00 DILM7DILM15; DILA DILM17DILM32 DILM40DIL65 DILM80; DILM95 DILM115; DIL150 DILM185DILM250 DILM300DILM500 DILM580DILM1000 DILH1400 DILH2000	4.6 4 8 16 26 3.5 4.3 4.3 7.5 7.5 7.5	543 472 944 1889 3069 413 508 508 885 885 1771	272 236 472 944 1535 207 254 254 443 443 885	434 378 756 1511 2456 331 406 406 708 708 708 1417	217 189 378 756 1228 165 203 203 354 354 708

Maximum permissible single control cable length for a rated control supply voltage of 230V and 120V and a maximum control supply voltage of 1.1 x U<sub>C</sub> for 50 Hz and 60 Hz mains frequency.

### 4. Measures to counteract excessive cable capacitance

Several solutions are possible if the engineering of an installation determines that the contactors will not drop out due to excessive cable capacitance:

- Use of contactors with higher coil sealing power
- Use of DC operated contactors
- Reduction of the control supply voltage (allow for voltage drop)
- Laying the supply cable near the command contacts
- An additional NC contact for twowire control and NO contact for three-wire control are used to short the coil.



Three-wire control

• Parallel switching of a resistance. The resistance is calculated as follows:

$$R = \frac{1000}{C_{L}} [\Omega] \quad C_{L} \text{ in } \mu \text{F}$$
 (4.1)

The power of the resistance is:

$$P = \frac{U_c^2}{R} \quad [W] \tag{4.2}$$

It must be taken into account that the resistor increases the total heat dissipation of the circuit.





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